

#### CNOSSOS-EU Railway noise versus The EU Interim Railway noise Standard Calculation Method II

13 October 2016

Union Internationale des Chemins de Fer Vienna

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- Introduction
- History
- Purpose field of application
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- Conclusions and recommendations



# The developments last 17 years

Harmonoise	1999 - 2004	Extensive research to come to an engineering method. Methods for calculations in a large number of meteo classes
Imagine	2004 - 2007	Further research on databases, aircraft noise and industrial noise
Good Practice Guide part 1	2004	Guidelines for doing calculations
Good Practice Guide part 2	2006	More extensive guidelines
CNOSSOS-EU	2008 - 2014	Harmonoise/Imagine was considered too extensive so it was desirable to establish a simpler method



The first objectives for Harmonoise in 1999 / 2000

The red and the green areas

Identification of 'Hot Spots'

The first investigation

Inaccuracy up to 3-5 dB(A)



Distinction between a poor quality and an acceptable noise environment

Further discussions to much higher accuracy



# Common method for EU

DG JRC published the final report on CNOSSOS-EU in August 2012 with detailed technical descriptions of engineering methods for:

- Source models for roads, rail and industry
- Point to point propagation model based upon NMPB 2008
- Aircraft noise mapping to be undertaken using ECAC Doc 29 3rd Edition, 2005

Directive of 19 May 2015 to have the CNOSSOS-EU method in Annex II of the END as the Common Method for use during round 4 of strategic noise mapping in 2022.





#### **Common method for EU**

CNOSSOS-EU should be designed to produce plausible noise maps showing plausible results.

For the purposes of CNOSSOS-EU, a parameter is considered essential if the range of values of the parameter can take yields variations in  $L_{den}$  or  $L_{night}$  of more than ±2.0 dB(A) 95% C.I.





# Standard Calculation Method II

The Dutch calculation method version of 1996

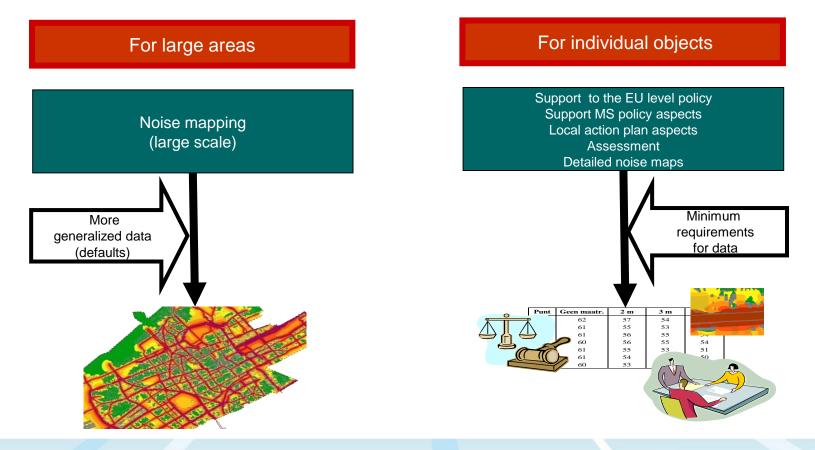
Standard Calculation Method II is the EU Interim Railway for noise mapping

By the way: In the Netherlands there are newer versions of this calculation method





# Fields of application





#### In common....

Defined in the frequency range from 63 Hz to 8 kHz

Calculations in octave bands

The A-weighted long term average sound level for day, evening and night is computed by summation over octave bands:

$$L_{\text{Aeq,T}} = 10 imes \lg \sum_{i=1} 10^{(L_{eq,T,i}+A_i)/10}$$

A<sub>i</sub> denotes the A-weighting correction according to IEC 61672-1
i = frequency band index
T is the time period corresponding to day, evening or night



CNOSSOS-EU Railway noise versus Standard Calculation Method II

**Noise Sources** 



#### Sources

#### SRM II

Physical source types:

- 1. rolling, impact and traction noise
- 2. aerodynamic noise
- 3. bridges

**CNOSSOS-EU** 

Physical source types:

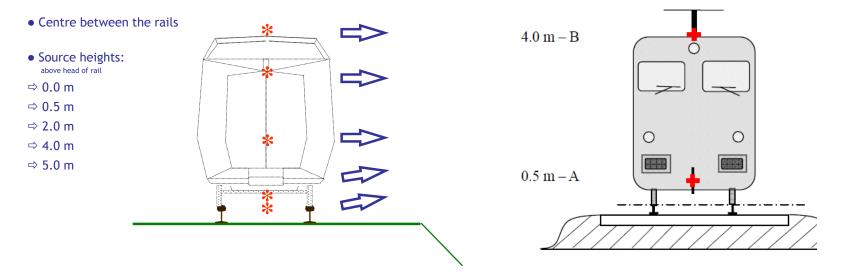
- 1. rolling and impact noise
- 2. curve squeal
- 3. traction noise
- 4. aerodynamic noise
- 5. additional effects (as bridges and shunting yards)



# Source positions

#### SRM II

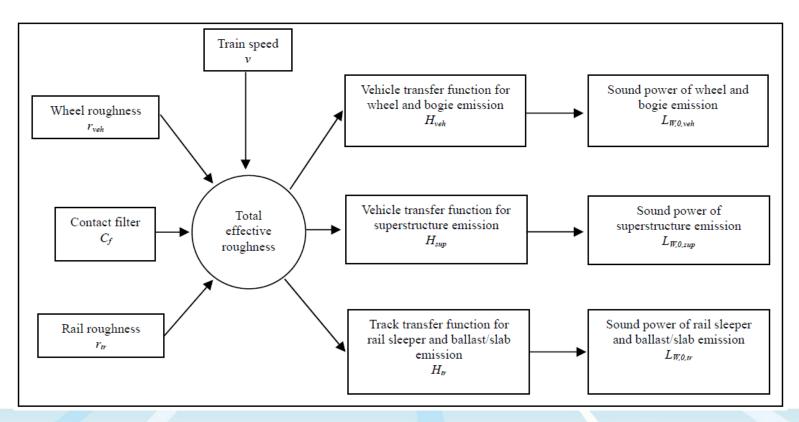
#### **CNOSSOS-EU**



Mind that the source positions also have direct relations to barrier attenuations !

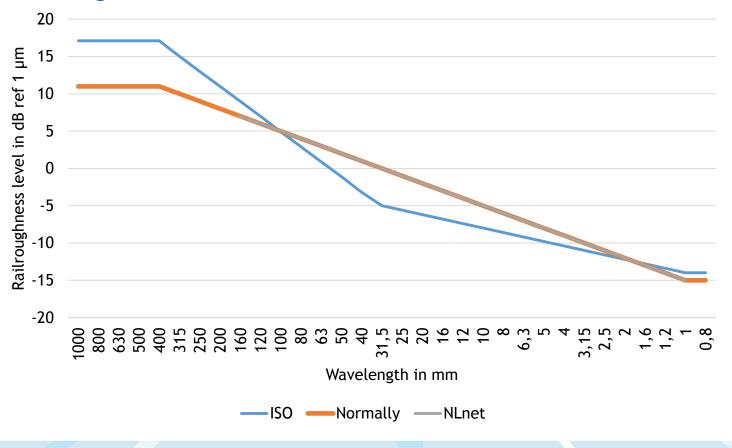


# Scheme of the use of the different roughness and transfer function definitions



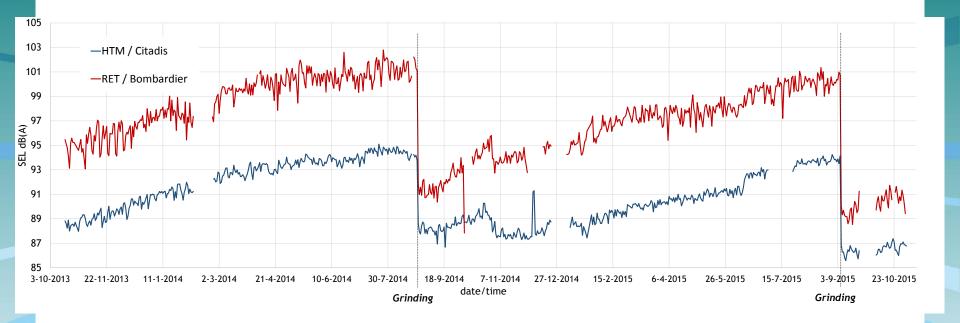


# Rail roughness





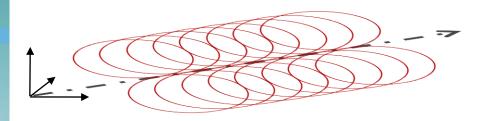
# Results over several years of light-rail vehicles



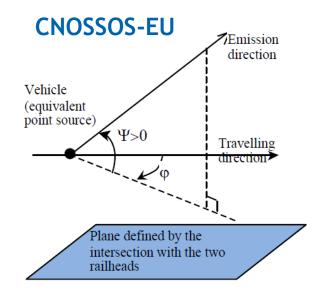


# Directivity

**SRM II** 



# *Dipole - COSIN function* on the horizontal directivity



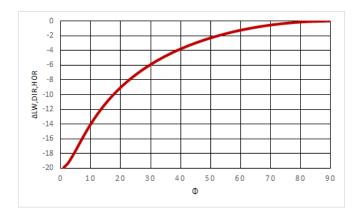
 $\Delta L_{W,dir,vert}$  is the vertical directivity correction function of  $\psi$ 

 $\textit{\Delta L}_{\textit{W},\textit{dir},\textit{hor}}$  is the horizontal directivity correction function of  $\phi$ 



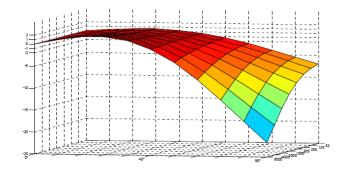
# **Directivity - default**

#### Horizontal low and high source

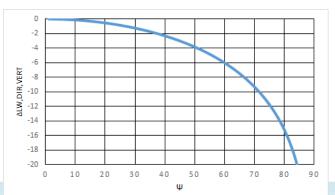


*Dipole - SIN function* on the horizontal directivity

#### Vertical low source - aerodynamic



#### Vertical high source - aerodynamic





#### Curve squeal noise

Adding to the rolling noise sound power spectra

- for at least a 50 m length of track
- for all frequencies

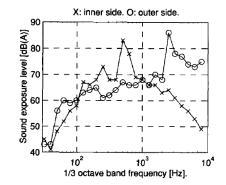


Figure 1.3: Curve squealing: spectrum of the sound exposure level. Single measurements made by van Leeuwen [64]

- 8 dB for R < 300 m
- 5 dB for 300 m < R < 500 m

#### Squeal noise is associated with the sources at 0,5 m (source A).

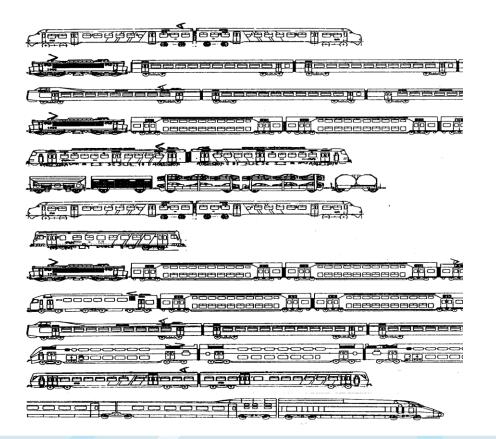


CNOSSOS-EU Railway noise versus Standard Calculation Method II

Input data aspects



# **SRM 2 - Predefined Train Categories**

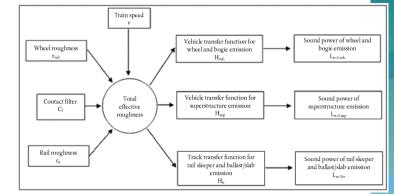




### The CNOSSOS-EU Rail source model

Complex source model depending on

- rolling noise (rail/wheel roughness)
- impact noise (crossings/switches/junctions)
- squeal (radius)
- traction noise
- aerodynamic noise
- directivity
- bridges etc.



The source model is in 1/3 octave, however for propagation and octaves are used

#### 2 source heights at 0.5 meter and 4.0 meter above the rail track

- Rolling noise: 0.5 meter
- Traction noise: 0.5 and 4.0 m
- Aerodynamic noise: 0.5 and 4.0 m
- Impact noise: 0.5 m
- Squeal noise: 0.5 m
  - Bridge noise: 0.5 m



# Rail conversion / input database table

Code	C Description	D B mash	E V max	F Weight	G Lenath	H Axles		J siaal⊡iamatarΩ	K WheelMeasur	L ProkoCodo	M Auto Lood	N	0 BefControl	P t RefRoughnes	Q	B
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		0						) large						U: (		
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	Example Vehicle 2	640					920			CastironBloc				2		2
NCF BB66400	Diesel loc	830					1100	· • • • • • • • • • • • • • • • • • • •		CastironBloc				6		3
SNCF CC72000	Diesel loc	2250					1140	· • • • • • • • • • • • • • • • • • • •		CastironBloc				6		4
RENFE Dioco	Diesel loc	1155					¥ 1000			CastironBloc				6		5
JS6400 Dloco	Diesel loc	1180					¥1000			CastironBloc				6		6
KOJ JT42CWR/Class66	Diesel loc	2200					3 1120			)ositeBlock-I			r :	6 4		7
IS DM 90 DMU	DMU	640					¥ 920			Disc-Non-Tre-				6		8
IS 1700 Eloco	ELoco	4560					1260			CastlronBloc				6		9
S mat 64 EMU	EMU	508	140	82			4 920	) large		CastlronBloc				6		0
MR Cat 1	Block braked passenger				26		ŧ	large		CastironBloc				6		0
MR Cat 2 (a)	ICM-III, ICR trailer, SNCF passenger, TEE				20	1	ł	large	none	CastlronBloc	k		3 (	6 3		0
IMR Cat 2 (b)	ICR 1700, DDM-1 1800 loco, Belgian locos				18		ł	large	none	CastironBloc	k.	(	S] (	6 (	3	9
MR Cat 3	Disc braked passenger trains				26		ŧ.	large	none	)isc-Non-Tre	ad	1	3 (	6 5	5 1	0
MR Cat 4	Block braked freight trains variable I and no.				1	1	1	large	none	CastironBloc	k.		3 (	6 (	3	0
MR Cat 5 (a)	DE1, DE2, DE3				25		Í.	large		CastironBloc				6	3	8
MR Cat 5 (b)	2200, 2300 locos				14		ł	large		CastironBloc					3	3
MR Cat 5 (c)	2400.2500 locos		••••••••••••••••••••••••••••••••••••••		1		l .	large		CastlronBloc				6		3
MR Cat 6	Diesel trains with disc brakes		•		20			large		Jisc-Non-Tre				6 6		8
MR Cat 7	Disc braked urban subway and rapid tram trains		••••••••••••••••••••••••••••••••••••••		1		2	medium		Jisc-Non-Tre				6		0
MR Cat 8 (a)	ICM IV, IRM		•		20		í	large		Disc-Non-Tre				6		0
MR Cat 8 (b)	DDM 2/3				20		[	large		CastironBloc						0
MR Cat 9 (a)	TGV PBA type, power car		•		20		t 4			CastironBloc				6		9
	TGV PBA type, trailer car adjacent to power		÷		20		* : 3	large		)isc-Non-Tre				6		0
RMR Cat 9 (b)					20		2	large		Disc-Non-Tre-				6 5		0
RMR Cat 9 (c)	TGV PBA types, other trailer cars	1	1		: 20		4:	large					s;	b; 5	D;	
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CNOSSOS-EU Railway noise versus Standard Calculation Method II

Propagation



# SRM 2 - Sound level in favorable conditions and a correction

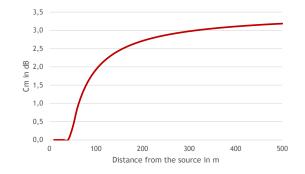
Receiver calculations are made according to the following steps:

1. for each propagation path the calculation of the attenuation in favorable conditions

2. calculation of the long-term sound level for each path by using  $C_M$ 

$$C_M = 3.5 - 35 \cdot \frac{h_{source} + h_{receiver}}{R}$$

3. accumulation of the long-term sound levels for all paths





# CNOSSOS - Sound level in homogeneous and in favorable conditions

Receiver calculations are made according to the following steps:

- 1. on each propagation path:
  - calculation of the attenuation in favorable conditions
  - calculation of the attenuation in homogeneous conditions

$$L_{LT} = 10 \times lg \left( p \cdot 10^{\frac{L_F}{10}} + (1 - p) \cdot 10^{\frac{L_H}{10}} \right)$$

- 2. calculation of the long-term sound level for each path by susing the percentage favorable (p %) and homogeneous conditions (100 p %)
- 3. accumulation of the long-term sound levels for all paths



# **CNOSSOS - Propagation**

$$L_{LT} = 10 \times \lg \left( p \cdot 10^{\frac{L_F}{10}} + (1-p) \cdot 10^{\frac{L_H}{10}} \right)$$
$$L_H = L_{w,o,dir} - (A_{div} + A_{atm} + A_{boundary,F})$$
$$L_F = L_{w,o,dir} - (A_{div} + A_{atm} + A_{boundary,H})$$

A<sub>div</sub> is the attenuation due to geometrical divergence
A<sub>atm</sub> is the attenuation due to atmospheric absorption
A<sub>boundary,F/H</sub> is the attenuation in favorable/homogeneous conditions. It contains the following:
A<sub>ground,F/H</sub> which is the attenuation due to the ground in favorable/homogeneous conditions
A<sub>dif,F/H</sub> which is the attenuation due to diffraction in favorable/homogeneous conditions



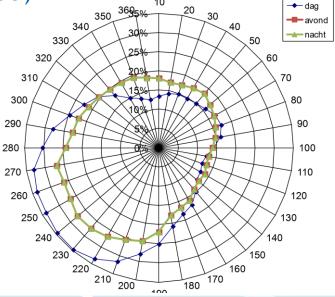
# **CNOSSOS - Propagation and meteo**

### 2 calculations

- Homogeneous: straight rays
- Favourable: curvature 8R (equivalent to ISO)

Method to calculate %<sub>favoured per period</sub>

This method replaces the  $\rm C_m$  correction according to ISO and the Dutch calculation method



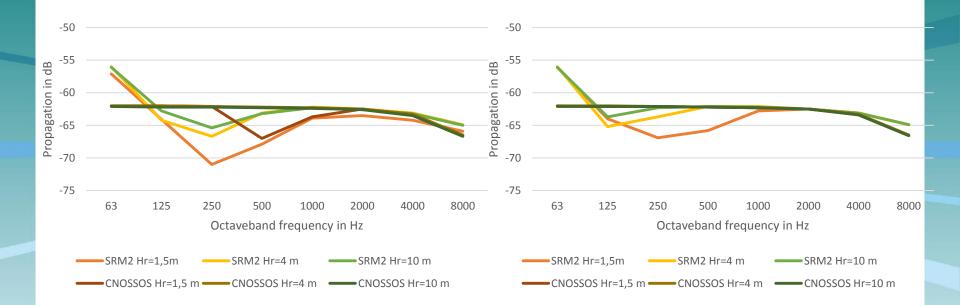


# G values for different types of ground

Description	Туре	(kPa · s/m²)	G value
Very soft (snow or moss-like)	А	12,5	1
Soft forest floor (short, dense heather-like or thick moss)	В	31,5	1
Uncompacted, loose ground (turf, grass, loose soil)	С	80	1
Normal uncompacted ground (forest floors, pasture field)	D	200	1
Compacted field and gravel (compacted lawns, park area)	E	500	0,7
Compacted dense ground (gravel road, car park)	F	2 000	0,3
Hard surfaces (most normal asphalt, con- crete)	G	20 000	0
Very hard and dense surfaces (dense as- phalt, concrete, water)	Н	200 000	0

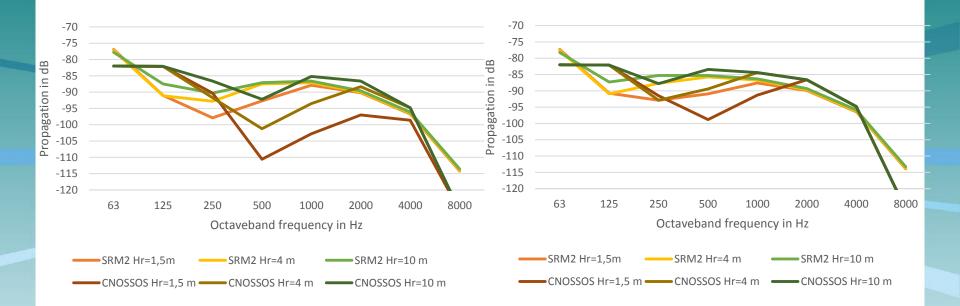


## Propagation to a microphone at 50 m



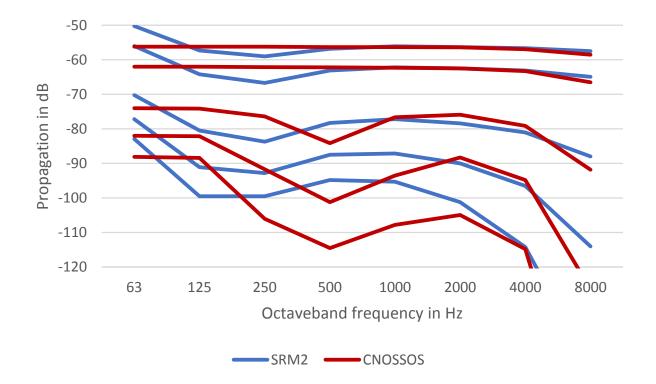


## Propagation to a microphone at 500 m



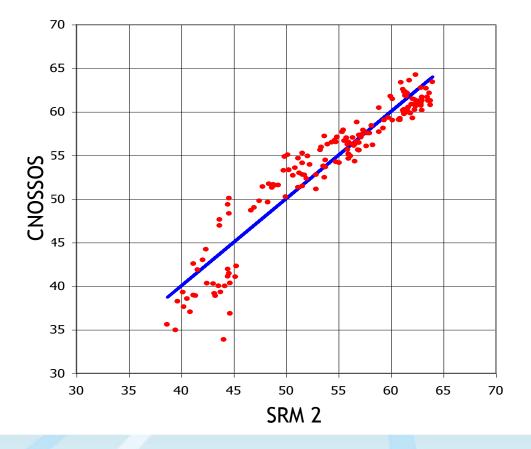


# Propagation of a source at 0,5 m height to a microphone at 25, 50, 200, 500, 1000 m, 4 m above the ground





# CNOSSOS - SRM 2





CNOSSOS-EU Railway noise versus Standard Calculation Method II

> Conclusions Recommendations



# Conclusions

- A simpler source model by using only two source heights
- In the source more aspects as traction noise and curve squeal
- Rail conversion tables
- Extra input data on meteo
- CNOSSOS will give
  - somewhat higher levels for reflective ground
  - somewhat lower levels for absorptive ground
- Source power determination should be according to inverse propagation calculation





### Recommendations

Define the field of application in your MS:

- $\checkmark$  Strategic noise maps and action plans
- ✓ Assessment and legislation

Check your emissions:

• Define your vehicles

Anticipate the public on new calculation results

- More reliable and more state-of-the-art
- What's in it for me
- What is the best method for reducing noise levels

Calculate round 3 (now 2018) with the old method and with CNOSSOS







# Thanks for your attention

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